

**Hooke's Law Shear Stresses**

$$\sigma = E \cdot \epsilon \quad \tau_{avg} = \frac{V}{A} \quad \tau = G \gamma \quad G = \frac{E}{2(1+\nu)} \quad \epsilon_x = \frac{\sigma_x - \nu(\sigma_y + \sigma_z)}{E}$$

**Poisson's Ratio**

$$\nu = -\frac{\epsilon_{lat}}{\epsilon_{long}}$$

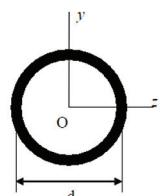
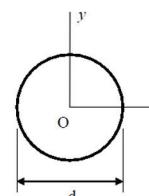
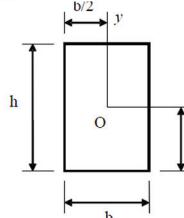
$$I_x = I_{x'} + A \cdot d_y^2$$

$$\delta = \sum \frac{PL}{EA}$$

volumetric strain

$$e = \frac{\Delta V}{V} = \epsilon_x + \epsilon_y + \epsilon_z = \frac{1-2\nu}{E} (\sigma_x + \sigma_y + \sigma_z)$$

$$e = -\frac{3(1-2\nu)}{E} p = -\frac{p}{K} \quad \text{with } K = \frac{E}{3(1-2\nu)}$$



General bending eq.

$$\sigma_z = \left( \frac{M_y I_{xx} - M_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) x + \left( \frac{M_x I_{yy} - M_y I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) y = \left( \frac{I_{yy} y - I_{xy} x}{I_{xx} I_{yy} - I_{xy}^2} \right) M_x + \left( \frac{I_{xx} x - I_{xy} y}{I_{xx} I_{yy} - I_{xy}^2} \right) M_y$$

 If  $I_{xy}=0$ 

$$\sigma_z = \frac{M_x}{I_{xx}} y + \frac{M_y}{I_{yy}} x$$

Neutral axis

$$\alpha = \arctan \left( \frac{M_y I_{xx} - M_x I_{xy}}{M_x I_{yy} - M_y I_{xy}} \right)$$

non-warping Neuber beams

$$p_R G t = \text{constant}$$

Airy

$$\sigma_x = \frac{\partial^2 \phi}{\partial y^2}, \quad \sigma_y = \frac{\partial^2 \phi}{\partial x^2}, \quad \tau_{xy} = -\frac{\partial^2 \phi}{\partial x \partial y}$$

Prandtl

$$\tau_{zy} = -\frac{\partial \phi}{\partial x} \quad \text{and} \quad \tau_{zx} = \frac{\partial \phi}{\partial y}$$

**Torsion Formulas (Circular shafts)**

$$\tau(\rho) = \frac{T \cdot \rho}{J} \quad \phi = \frac{TL}{GJ} \quad \phi = \int_0^L \frac{T(x)}{J(x)G} dx$$

**Flexure Formula**

$$\sigma = -\frac{My}{I}$$

**Torsion Formulas (Thin-walled shafts)**

$$\tau_{avg} = \frac{T}{2tA_m} \quad q = \frac{T}{2A_m} \quad \phi = \frac{TL}{4A_m^2 G} \cdot \int_0^{L_m} \frac{1}{t} ds$$

**Shear Formula**

$$\tau = \frac{VQ}{It} \quad Q = \bar{y}' \cdot A'$$

**Open cross sections**

$$\tau_{zs} = \frac{2n}{J} T = 2Gn \frac{d\theta}{dz} \quad \text{at edges} \quad n = t/2 \quad J = \frac{1}{3} \int t^3 ds \quad \text{where also} \quad T = GJ \frac{d\theta}{dz}$$

Torsion over several boxes

$$T_R = 2A_R q_R \quad \text{with} \quad \sum_{R=1}^N T_R = T$$

$$\frac{d\theta}{dz} = \frac{1}{2A_R G} \oint_R \frac{q}{t} ds \quad B_1 = \frac{t_D b}{6} \left( 2 + \frac{\sigma_2}{\sigma_1} \right) \quad \text{and} \quad B_2 = \frac{t_D b}{6} \left( 2 + \frac{\sigma_1}{\sigma_2} \right)$$

Trusses

 kin. indet.  $m+r < 2n$ 

 stat. indet.  $m+r = 2n$ 

 degree of stat. indet.  $d = m+r-2n$ 

n=joints

m=members

r=reaction forces

Simplifying a piece of skin into two beams

**Castigliano's theorem**
**Maxwell**

$$U = \int_0^l P d\delta = \int_0^l \frac{P}{k} dP = \frac{P^2}{2k} = \frac{P^2 L}{2AE} \quad f_{BA} = f_{AB}$$

**Von Misses stress**

$$Y = \sqrt{\frac{1}{2} \left[ (\sigma_x - \sigma_y)^2 + (\sigma_y - \sigma_z)^2 + (\sigma_z - \sigma_x)^2 \right] + 3\tau_{xy}^2 + 3\tau_{yz}^2 + 3\tau_{xz}^2}$$

Type	Displacement	Energy
Tension/Compression Bar	$d\delta = \frac{F dx}{AE}$	$dU = \frac{1}{2} F d\delta = \frac{F^2 dx}{2AE}$
Torsion Bar	$d\phi = \frac{T dx}{GJ}$	$dU = \frac{1}{2} T d\phi = \frac{T^2 dx}{2GJ}$
Bending Beam	$d\theta = \frac{M dx}{EI}$	$dU = \frac{1}{2} M d\theta = \frac{M^2 dx}{2EI}$
Shear Beam	$\gamma = \frac{VQ}{ItG} \approx \frac{V}{AG}$	$dU = \frac{1}{2} V \gamma dx = \frac{V^2 Q dx}{2ItG} \approx \frac{V^2 dx}{2AG}$

**Mohr**

$$\tan 2\theta_{m\sigma} = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

$$\tan 2\theta_{m\tau} = -\frac{\sigma_x - \sigma_y}{2\tau_{xy}}$$

$$\tau_{max} = R = \frac{\sigma_I - \sigma_{II}}{2}$$

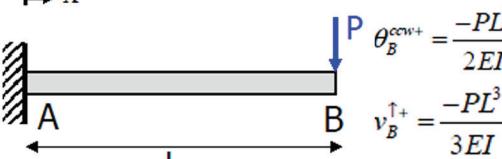
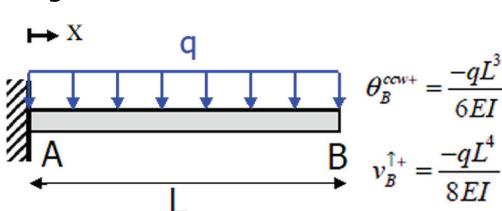
 Statics  
tbv diagrams

$$q = EI u'''$$

$$V = EI u''$$

$$M = EI u''$$

$$\theta = u'$$



$$\sigma_I = \sigma_{av} + R \quad \text{and} \quad \sigma_{II} = \sigma_{av} - R$$

$$\delta = u$$