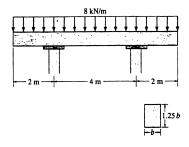
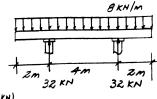
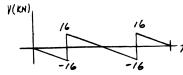
11-1 The simply supported beam is made of timber that has an allowable bending stress of $\sigma_{\rm allow} = 6.5$ MPa and an allowable shear stress of $\tau_{\rm allow} = 500$ kPa. Determine its dimensions if it is to be rectangular and have a height-towidth ratio of 1.25.









M (MM)

$$I_x = \frac{1}{12}(b)(1.25b)^3 = 0.16276b^4$$

$$Q_{\text{max}} = \bar{y}'A' = (0.3125b)(0.625b)(b) = 0.1953125b^3$$

Assume bending moment controls:

$$M_{\text{max}} = 16 \text{ kN} \cdot \text{m}$$

$$\sigma_{\text{allow}} = \frac{M_{\text{max}} c}{I}$$

$$6.5(10^6) = \frac{16(10^3)(0.625b)}{0.16276b^4}$$

$$b = 0.21143$$
m = 211 mm Ans
h = 1.25b = 264mm Ans

Check shear:

$$Q_{\text{max}} = 1.846159(10^{-3}) \text{ m}^3$$

 $I = 0.325248(10^{-3})\text{m}^4$

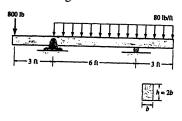
$$I = 0.325248(10^{-3})\text{m}^4$$

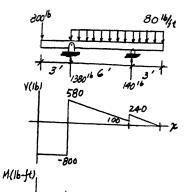
$$\tau_{\text{max}} = \frac{VQ_{\text{max}}}{It} = \frac{16(10^3)(1.846159)(10^{-3})}{0.325248(10^{-3})(0.21143)} = 429 \text{ kPa} < 500 \text{ kPa} \qquad \text{OK}$$

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11-2. The beam is made of Douglas fir having an allowable bending stress of $\sigma_{\rm allow} = 1.1$ ksi and an allowable shear stress of $\tau_{\rm allow} = 0.70$ ksi. Determine the width b of the beam if the height h = 2b.





2400

$$I_x = \frac{1}{12}(b)(2b)^3 = 0.6667 \ b^4$$

$$Q_{\text{max}} = \bar{y}'A' = (0.5b)(b)(b) = 0.5b^3$$

Assume bending moment controls:

$$M_{\text{max}} = 2400 \text{ lb} \cdot \text{ft}$$

$$\sigma_{\text{allow}} = \frac{M_{\text{max}} c}{I}$$

$$1100 = \frac{2400(12)(b)}{0.6667b^4}$$

$$b = 3.40 \text{ in.}$$
 Ans

Check shear:

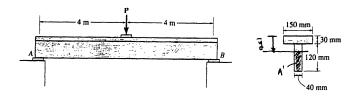
$$Q_{\max} = 19.65 \text{ in}^3$$

$$I = 89.09 \text{ in}^4$$

$$\tau_{\text{max}} = \frac{VQ_{\text{max}}}{It} = \frac{800(19.65)}{89.09(3.40)} = 51.9 \text{ psi} < 700 \text{ psi}$$
 OK

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11-3 The timber beam is to be loaded as shown. If the ends support only vertical forces, determine the greatest magnitude of **P** that can be applied. $\sigma_{\text{allow}} = 25 \text{ MPa}, \tau_{\text{allow}} = 700 \text{ kPa}.$



$$\bar{y} = \frac{(0.015)(0.150)(0.03) + (0.09)(0.04)(0.120)}{(0.150)(0.03) + (0.04)(0.120)} = 0.05371 \text{ m}$$

$$I = \frac{1}{12}(0.150)(0.03)^3 + (0.15)(0.03)(0.05371 - 0.015)^2 + \frac{1}{12}(0.04)(0.120)^3 + (0.04)(0.120)(0.09 - 0.05371)^2 = 19.162(10^{-6}) \text{ m}^4$$

Maximum moment at center of beam:

$$M_{\text{max}} = \frac{P}{2}(4) = 2P$$

$$\sigma = \frac{Mc}{I}; \qquad 25(10^6) = \frac{(2P)(0.15 - 0.05371)}{19.162(10^{-6})}$$

$$P = 2.49 \text{ kN}$$

Maximum shear at end of beam:

$$V_{\text{max}} = \frac{P}{2}$$

$$\tau = \frac{VQ}{It}; \qquad 700(10^3) = \frac{\left[\frac{1}{2}(0.15 - 0.05371)(0.04)(0.15 - 0.05371)\right]}{19.162(10^{-6})}$$

$$P = 145 \text{ kN}$$

Thus,

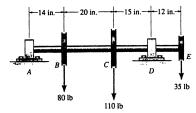
$$P = 2.49 \text{ kN}$$
 Ans

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*11-4 Draw the shear and moment diagrams for the shaft, and determine its required diameter to the nearest $\frac{1}{4}$ in. if $\sigma_{\text{allow}} = 7$ ksi and $\tau_{\text{allow}} = 3$ ksi. The bearings at A and D exert only vertical reactions on the shaft. The loading is applied to the pulleys at B, C, and E.



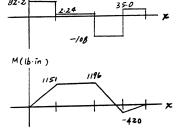
∀(1b)



$$7(10^3) = \frac{1196 c}{\frac{\pi}{a}c^4};$$
 $c = 0.601 in.$

$$d = 2c = 1.20 \text{ in.}$$

Use
$$d = 1.25$$
 in. Ans



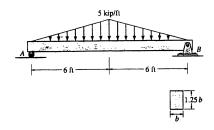
Check shear:

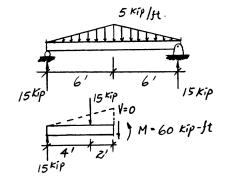
$$\tau_{\max} = \frac{V_{\max}Q}{It} = \frac{108(\frac{4(0.625)}{3\pi})(\pi)(\frac{0.625^2}{2})}{\frac{\pi}{4}(0.625)^4(1.25)} = 117 \text{ psi} < 3 \text{ ksi} \qquad \text{OK}$$

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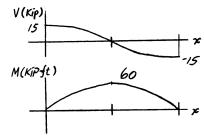
11-5 The simply supported beam is made of timber that has an allowable bending stress of $\sigma_{\rm allow}=960$ psi and an allowable shear stress of $\tau_{\rm allow}=75$ psi. Determine its dimensions if it is to be rectangular and have a height-to-width ratio of 1.25.





$$I = \frac{1}{12}(b)(1.25b)^3 = 0.16276b^4$$

$$S_{\text{req'd}} = \frac{I}{c} = \frac{0.16276b^4}{0.625b} = 0.26042b^3$$



Assume bending moment controls:

$$M_{\text{max}} = 60 \text{ kip} \cdot \text{ft}$$

$$\sigma_{\text{allow}} = \frac{M_{\text{max}}}{S_{\text{req'd}}}$$

$$960 = \frac{60(10^3)(12)}{0.26042 \ b^3}$$

$$b = 14.2 \text{ in.}$$

Check shear

$$\tau_{\text{max}} = \frac{1.5V}{A} = \frac{1.5(15)(10^3)}{(14.2)(1.25)(14.2)} = 88.9 \text{ psi} > 75 \text{ psi}$$
 NC

Shear controls:

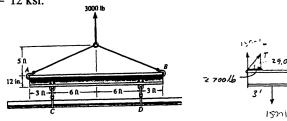
$$\tau_{\text{allow}} = \frac{1.5V}{A} = \frac{1.5(15)(10^3)}{(b)(1.25b)}$$

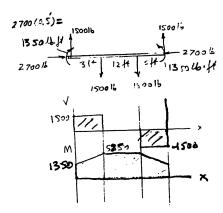
$$b = 15.5 \text{ in.}$$
 Ans

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11-6. The spreader beam AB is used to lift slowly the 3000-lb pipe that is centrally located on the straps at C and D. If the beam is a W 12 \times 45, determine if it can safely support the load. The allowable bending stress is $\sigma_{\rm allow} = 22 \, {\rm ksi}$ and the allowable shear stress is $\tau_{\rm allow} = 12 \, {\rm ksi}$.





$$h = \frac{1500}{\tan 29.055^{\circ}} = 2700 \text{ lb}$$

$$\sigma = \frac{M}{S}; \qquad \sigma = \frac{5850(12)}{58.1} = 1.21 \text{ ksi} < 22 \text{ ksi} \qquad \text{OK}$$

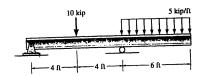
$$\tau = \frac{V}{A_{web}}; \qquad \tau = \frac{1500}{(12.06)(0.335)} = 371 \text{ psi} < 12 \text{ ksi} \qquad \text{O}$$

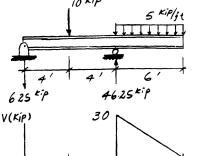
Yes.

Ans

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11-7 Select the lightest-weight steel wide-flange beam from Appendix B that will safely support the loading shown. The allowable bending stress is $\sigma_{\rm allow}=24$ ksi and the allowable shear stress is $\tau_{\rm allow}=14$ ksi.





-6.25 -16.25 M(Kip-ft)

Assume bending moment controls.

$$M_{\text{max}} = 90 \text{ kip · ft}$$

$$S_{\text{req'd}} = \frac{M_{\text{max}}}{\sigma_{\text{allow}}} = \frac{90(12)}{24} = 45 \text{ in}^3$$

M(Kip-ft)
- 25

Select a W 16 x 31

$$S_x = 47.5 \text{ in}^3$$
 $d = 15.88 \text{ in.}$ $t_w = 0.275 \text{ in.}$

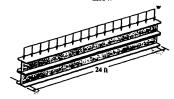
Check shear:

$$\tau_{\text{max}} = \frac{V_{\text{max}}}{A_{\text{w}}} = \frac{30}{(15.88)(0.275)} = 6.87 \text{ ksi} < 14 \text{ ksi}$$
 OK

Use W 16 x 31 Ans

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*11-8. The simply supported beam is composed of two W 12×22 sections built up as shown. Determine the maximum uniform loading w the beam will support if the allowable bending stress is $\sigma_{\text{allow}} = 22 \text{ ksi}$ and the allowable shear stress is $\tau_{\text{allow}} = 14 \text{ ksi.}$



Section properties: For W 12 x 22 (d = 12.31 in. $I_x = 156$ in $I_w = 0.260$ in. A = 6.48 in $I_w = 0.260$ in. $I_w = 0.260$ in. $I_w = 0.260$ in. $I_w = 0.260$ in.

$$I = 2[156 + 6.48(\frac{12.31}{2})^2] = 802.98 \text{ in}^4$$

$$S = \frac{I}{c} = \frac{802.98}{12.31} = 65.23 \, \text{in}^3$$

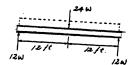
Maximum Loading: Assume moment controls. $M = \sigma_{\rm allow} S$

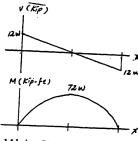
$$(72 w)(12) = 22(65.23)$$

$$w = 1.66 \, \text{kip} / \, \text{ft}$$

Check Shear: (Neglect area of flanges.)
$$T_{\text{max}} = V_{\text{max}}$$
12(1.66)

$$\tau_{\text{max}} = \frac{V_{\text{max}}}{A_{\text{w}}} = \frac{12(1.66)}{2(12.31)(0.26)} = 3.11 \text{ ksi} < \tau_{\text{allow}} = 14 \text{ ksi}$$
 OK





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