

Section 3.9

2. We have $\sin(\alpha \pm \beta) = \sin \alpha \cos \beta \pm \cos \alpha \sin \beta$. Subtracting the two identities, we obtain $\sin(\alpha + \beta) - \sin(\alpha - \beta) = 2 \cos \alpha \sin \beta$. Setting $\alpha + \beta = 7t$ and $\alpha - \beta = 6t$, $\alpha = 6.5t$ and $\beta = 0.5t$. Hence $\sin 7t - \sin 6t = 2 \sin \frac{t}{2} \cos \frac{13t}{2}$.

3. Consider the trigonometric identity $\cos(\alpha \pm \beta) = \cos \alpha \cos \beta \mp \sin \alpha \sin \beta$. Adding the two identities, we obtain $\cos(\alpha - \beta) + \cos(\alpha + \beta) = 2 \cos \alpha \cos \beta$. Comparing the expressions, set $\alpha + \beta = 2\pi t$ and $\alpha - \beta = \pi t$. Hence $\alpha = 3\pi t/2$ and $\beta = \pi t/2$. Upon substitution, we have $\cos(\pi t) + \cos(2\pi t) = 2 \cos(3\pi t/2) \cos(\pi t/2)$.

4. Adding the two identities $\sin(\alpha \pm \beta) = \sin \alpha \cos \beta \pm \cos \alpha \sin \beta$, it follows that $\sin(\alpha - \beta) + \sin(\alpha + \beta) = 2 \sin \alpha \cos \beta$. Setting $\alpha + \beta = 4t$ and $\alpha - \beta = 3t$, we have $\alpha = 7t/2$ and $\beta = t/2$. Hence $\sin 3t + \sin 4t = 2 \sin(7t/2) \cos(t/2)$.

6. Using *mks* units, the spring constant is $k = 5(9.8)/0.1 = 490 \text{ N/m}$, and the damping coefficient is $\gamma = 2/0.04 = 50 \text{ N-sec/m}$. The equation of motion is

$$5u'' + 50u' + 490u = 10 \sin(t/2).$$

The initial conditions are $u(0) = 0 \text{ m}$ and $u'(0) = 0.03 \text{ m/s}$.

8(a). The homogeneous solution is $u_c(t) = Ae^{-5t} \cos \sqrt{73}t + Be^{-5t} \sin \sqrt{73}t$. Based on the method of *undetermined coefficients*, the particular solution is

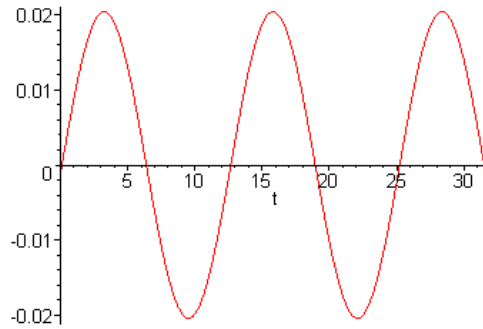
$$U(t) = \frac{1}{153281} [-160 \cos(t/2) + 3128 \sin(t/2)].$$

Hence the general solution of the ODE is $u(t) = u_c(t) + U(t)$. Invoking the initial conditions, we find that $A = 160/153281$ and $B = 383443\sqrt{73}/1118951300$. Hence the response is

$$u(t) = \frac{1}{153281} \left[160 e^{-5t} \cos \sqrt{73}t + \frac{383443\sqrt{73}}{7300} e^{-5t} \sin \sqrt{73}t \right] + U(t).$$

(b). $u_c(t)$ is the transient part and $U(t)$ is the steady state part of the response.

(c).



(d). Based on Eqs. (9) and (10), the amplitude of the forced response is given by $R = 2/\Delta$, in which

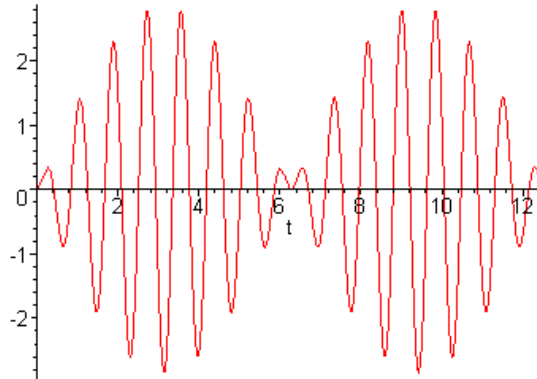
$$\Delta = \sqrt{25(98 - \omega^2)^2 + 2500\omega^2}.$$

The maximum amplitude is attained when Δ is a *minimum*. Hence the amplitude is maximum at $\omega = 4\sqrt{3}$ rad/s.

9. The spring constant is $k = 12$ lb/ft and hence the equation of motion is

$$\frac{6}{32}u'' + 12u = 4 \cos 7t,$$

that is, $u'' + 64u = \frac{64}{3} \cos 7t$. The initial conditions are $u(0) = 0$ ft, $u'(0) = 0$ fps. The general solution is $u(t) = A \cos 8t + B \sin 8t + \frac{64}{45} \cos 7t$. Invoking the initial conditions, we have $u(t) = -\frac{64}{45} \cos 8t + \frac{64}{45} \cos 7t = \frac{128}{45} \sin(t/2) \sin(15t/2)$.



12. The equation of motion is

$$2u'' + u' + 3u = 3 \cos 3t - 2 \sin 3t.$$

Since the system is *damped*, the steady state response is equal to the particular solution. Using the method of *undetermined coefficients*, we obtain

$$u_{ss}(t) = \frac{1}{6}(\sin 3t - \cos 3t).$$

Further, we find that $R = \sqrt{2}/6$ and $\delta = \arctan(-1) = 3\pi/4$. Hence we can write $u_{ss}(t) = \frac{\sqrt{2}}{6}\cos(3t - 3\pi/4)$.

13. The amplitude of the steady-state response is given by

$$R = \frac{F_0}{\sqrt{m^2(\omega_0^2 - \omega^2)^2 + \gamma^2 \omega^2}}.$$

Since F_0 is constant, the amplitude is *maximum* when the denominator of R is *minimum*. Let $z = \omega^2$, and consider the function $f(z) = m^2(\omega_0^2 - z)^2 + \gamma^2 z$. Note that $f(z)$ is a quadratic, with *minimum* at $z = \omega_0^2 - \gamma^2/2m^2$. Hence the amplitude R attains a maximum at $\omega_{max}^2 = \omega_0^2 - \gamma^2/2m^2$. Furthermore, since $\omega_0^2 = k/m$, and therefore

$$\omega_{max}^2 = \omega_0^2 \left[1 - \frac{\gamma^2}{2km} \right].$$

Substituting $\omega^2 = \omega_{max}^2$ into the expression for the amplitude,

$$\begin{aligned} R &= \frac{F_0}{\sqrt{\gamma^4/4m^2 + \gamma^2(\omega_0^2 - \gamma^2/2m^2)}} \\ &= \frac{F_0}{\sqrt{\omega_0^2 \gamma^2 - \gamma^4/4m^2}} \\ &= \frac{F_0}{\gamma \omega_0 \sqrt{1 - \gamma^2/4mk}}. \end{aligned}$$

14(a). The forced response is $u_{ss}(t) = A\cos \omega t + B\sin \omega t$. The constants are obtained by the method of *undetermined coefficients*. That is, comparing the coefficients of $\cos \omega t$ and $\sin \omega t$, we find that

$$-m\omega^2 A + \gamma\omega B + kA = F_0, \text{ and } -m\omega^2 B - \gamma\omega A + kB = 0.$$

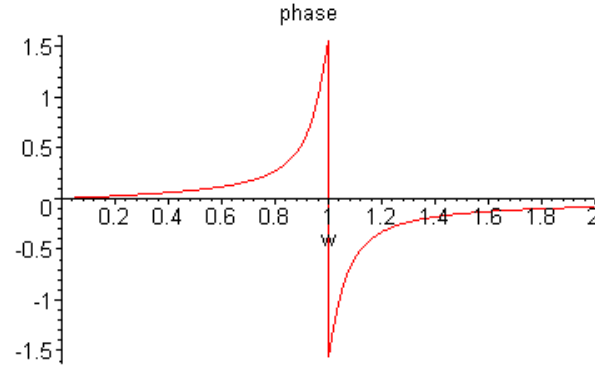
Solving this system results in

$$A = m(\omega_0^2 - \omega^2)/\Delta \quad \text{and} \quad B = \gamma\omega/\Delta,$$

in which $\Delta = \sqrt{m^2(\omega_0^2 - \omega^2)^2 + \gamma^2 \omega^2}$. It follows that

$$\tan \delta = B/A = \frac{\gamma\omega}{m(\omega_0^2 - \omega^2)}.$$

(b). Here $m = 1$, $\gamma = 0.125$, $\omega_0 = 1$. Hence $\tan \delta = 0.125\omega/(1 - \omega^2)$.

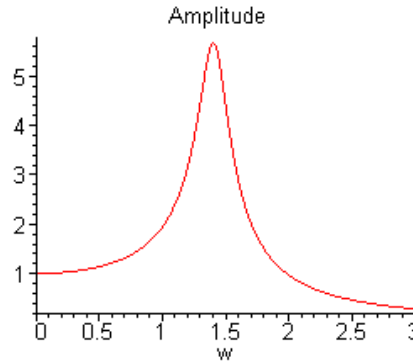


17(a). Here $m = 1$, $\gamma = 0.25$, $\omega_0^2 = 2$, $F_0 = 2$. Hence $u_{ss}(t) = \frac{2}{\Delta} \cos(\omega t - \delta)$, where $\Delta = \sqrt{(2 - \omega^2)^2 + \omega^2/16} = \frac{1}{4} \sqrt{64 - 63\omega^2 + 16\omega^4}$, and $\tan \delta = \frac{\omega}{4(2 - \omega^2)}$.

(b). The amplitude is

$$R = \frac{8}{\sqrt{64 - 63\omega^2 + 16\omega^4}}.$$

(c).



(d). See Prob. 13. The amplitude is maximum when the denominator of R is minimum. That is, when $\omega = \omega_{max} = 3\sqrt{14}/8 \approx 1.4031$. Hence $R(\omega = \omega_{max}) = 64/\sqrt{127}$.

18(a). The homogeneous solution is $u_c(t) = A \cos t + B \sin t$. Based on the method of *undetermined coefficients*, the particular solution is

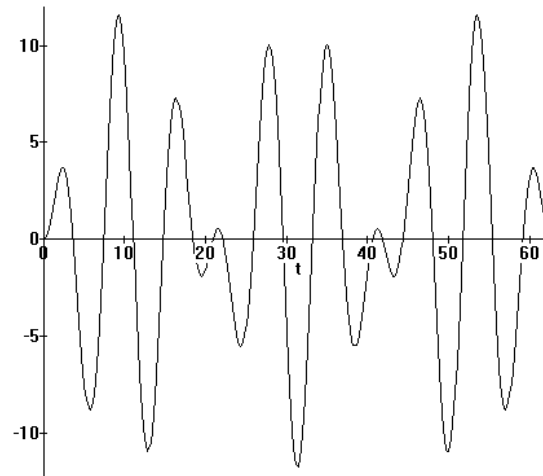
$$U(t) = \frac{3}{1 - \omega^2} \cos \omega t.$$

Hence the general solution of the ODE is $u(t) = u_c(t) + U(t)$. Invoking the initial conditions, we find that $A = 3/(\omega^2 - 1)$ and $B = 0$. Hence the response is

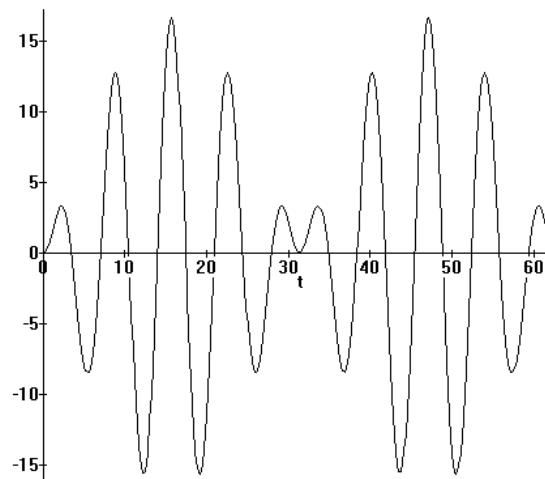
$$u(t) = \frac{3}{1 - \omega^2} [\cos \omega t - \cos t].$$

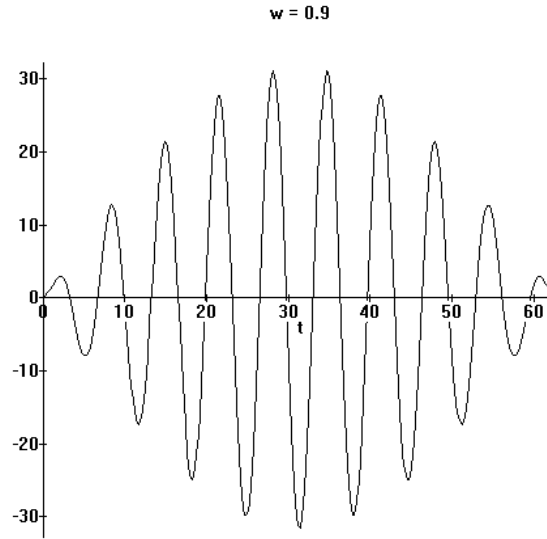
(b).

$\omega = 0.7$



$\omega = 0.8$





Note that

$$u(t) = \frac{6}{1 - \omega^2} \sin \left[\frac{(1 - \omega)t}{2} \right] \sin \left[\frac{(\omega + 1)t}{2} \right].$$

19(a). The homogeneous solution is $u_c(t) = A \cos t + B \sin t$. Based on the method of *undetermined coefficients*, the particular solution is

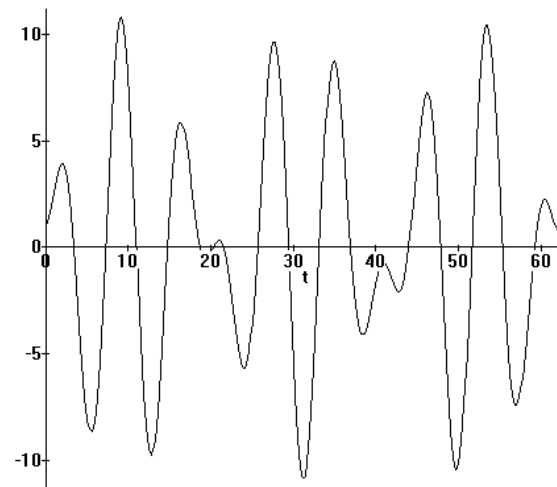
$$U(t) = \frac{3}{1 - \omega^2} \cos \omega t.$$

Hence the general solution is $u(t) = u_c(t) + U(t)$. Invoking the initial conditions, we find that $A = (\omega^2 + 2)/(\omega^2 - 1)$ and $B = 1$. Hence the response is

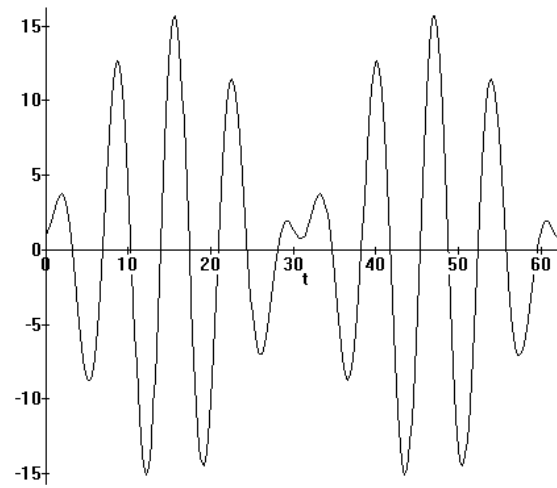
$$u(t) = \frac{1}{1 - \omega^2} [3 \cos \omega t - (\omega^2 + 2) \cos t] + \sin t.$$

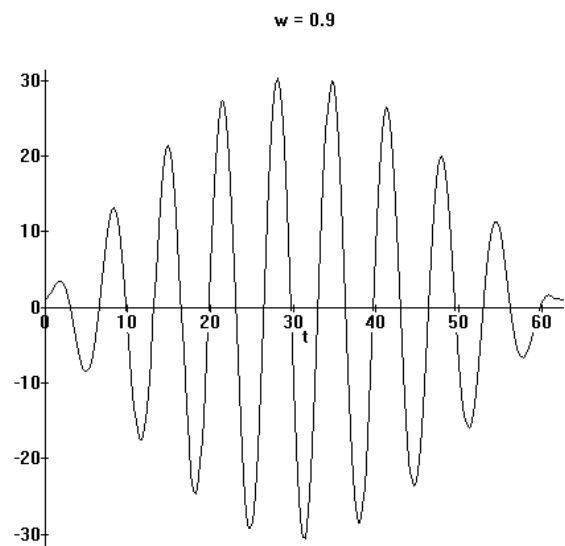
(b.)

$w = 0.7$



$w = 0.8$

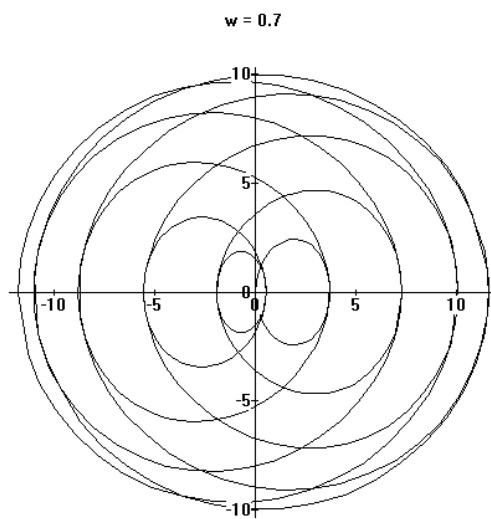


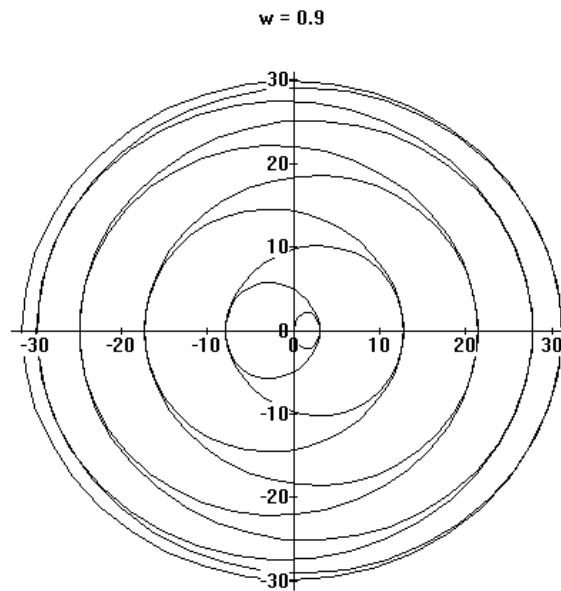
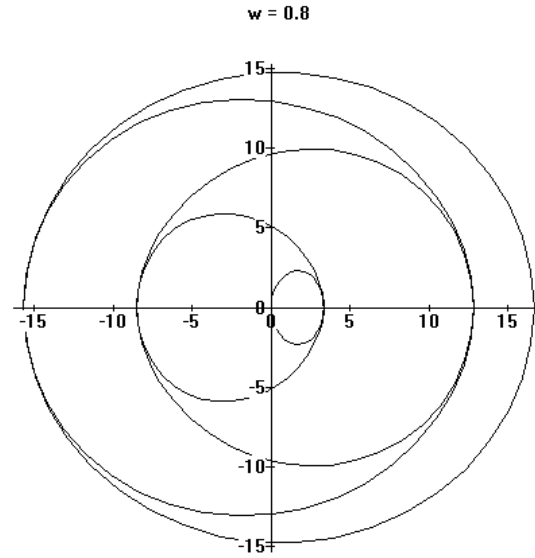


Note that

$$u(t) = \frac{6}{1 - \omega^2} \sin \left[\frac{(1 - \omega)t}{2} \right] \sin \left[\frac{(\omega + 1)t}{2} \right] + \cos t + \sin t.$$

20.





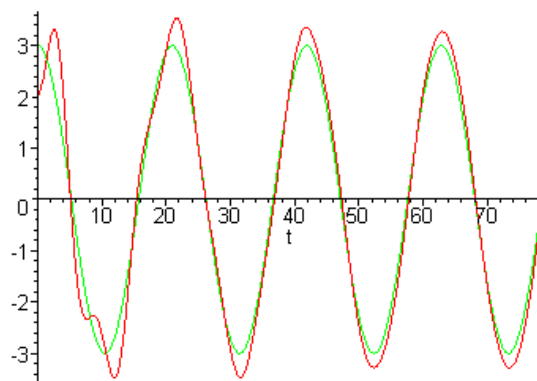
21. The general solution is $u(t) = u_c(t) + U(t)$, in which

$$u_c(t) = e^{-t/16} \left[-\frac{171358}{132721} \cos \frac{\sqrt{255}}{16} t - \frac{257758}{132721 \sqrt{255}} \sin \frac{\sqrt{255}}{16} t \right]$$

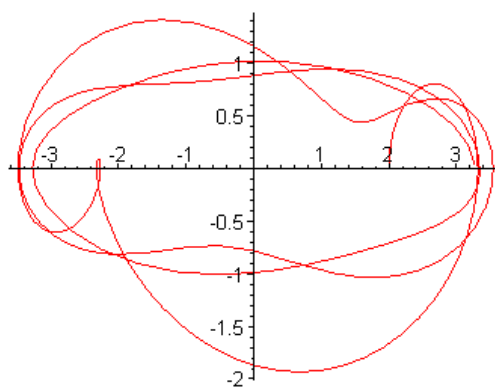
and

$$U(t) = \frac{1}{132721} [436800 \cos(.3t) + 18000 \sin(.3t)].$$

(a).



(b).



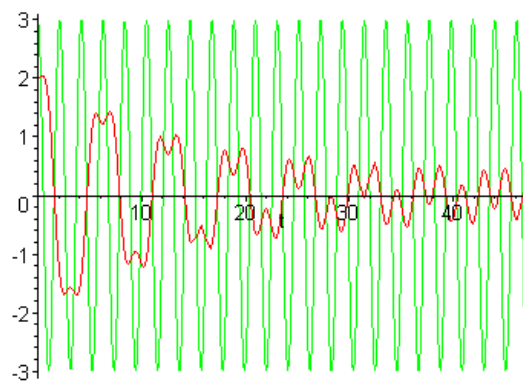
23. The general solution is $u(t) = u_c(t) + U(t)$, in which

$$u_c(t) = e^{-t/16} \left[\frac{9746}{4105} \cos \frac{\sqrt{255}}{16} t + \frac{1258}{821\sqrt{255}} \sin \frac{\sqrt{255}}{16} t \right]$$

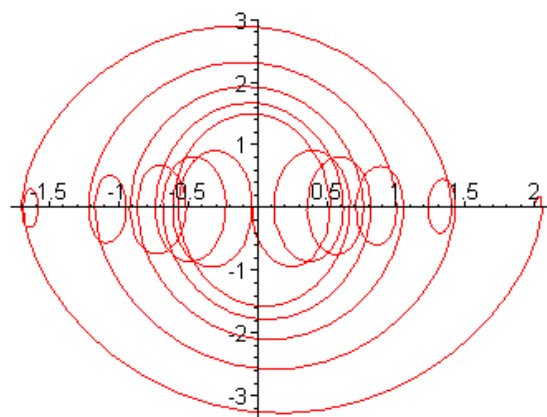
and

$$U(t) = \frac{1}{4105} [-1536 \cos(3t) + 72 \sin(3t)].$$

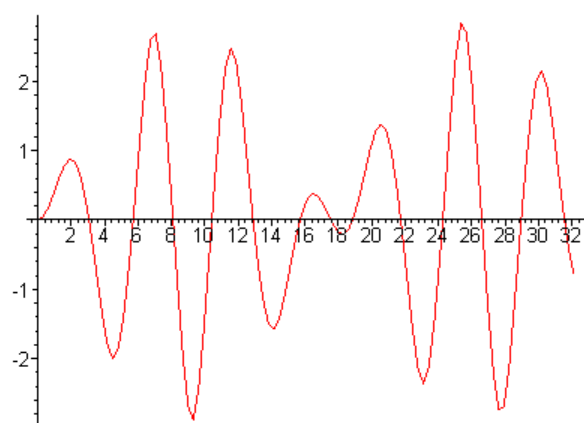
(a).



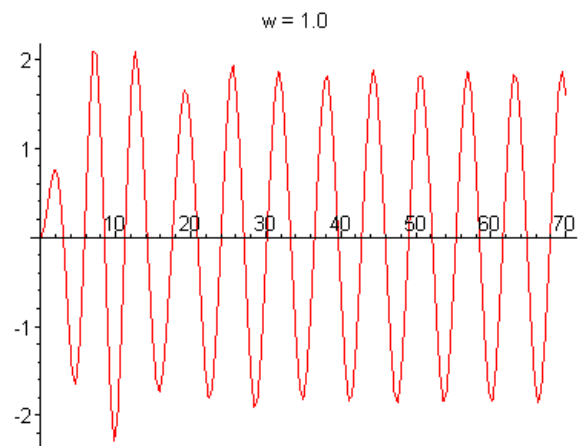
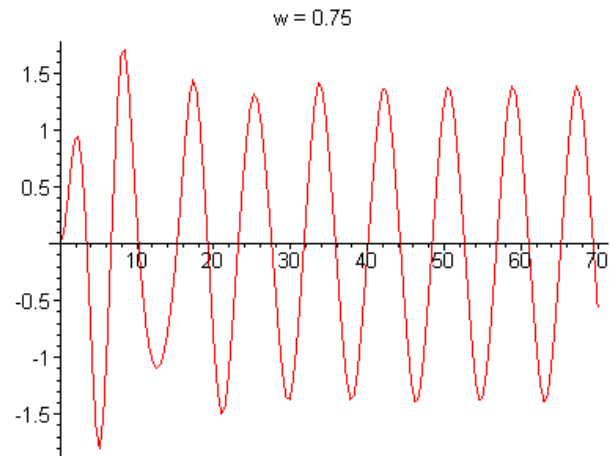
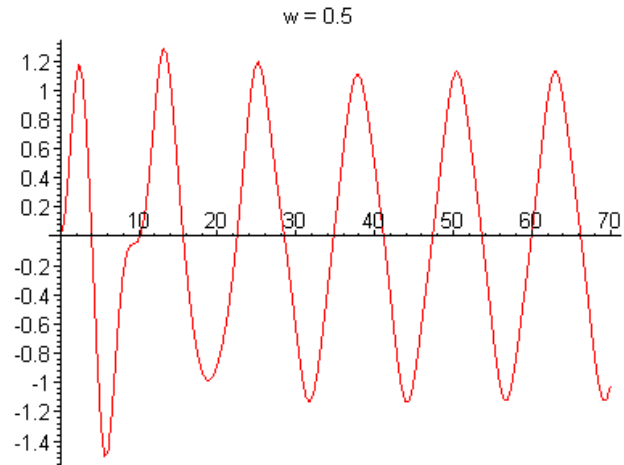
(b).

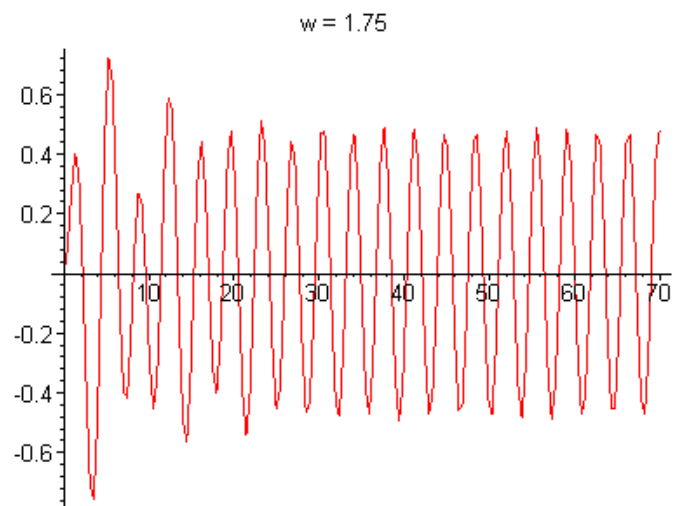
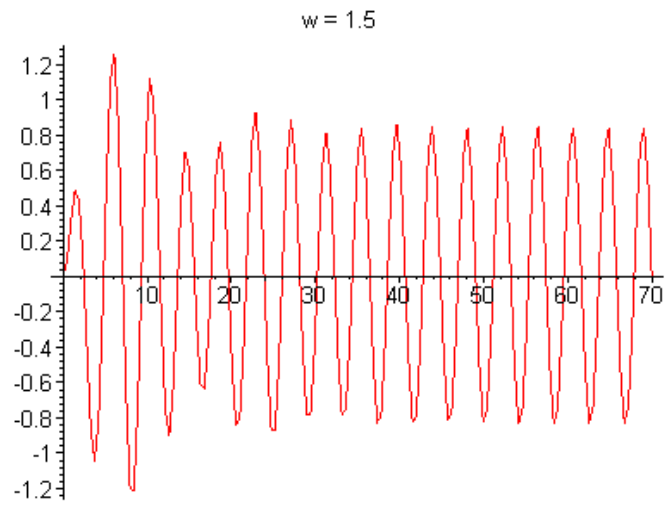
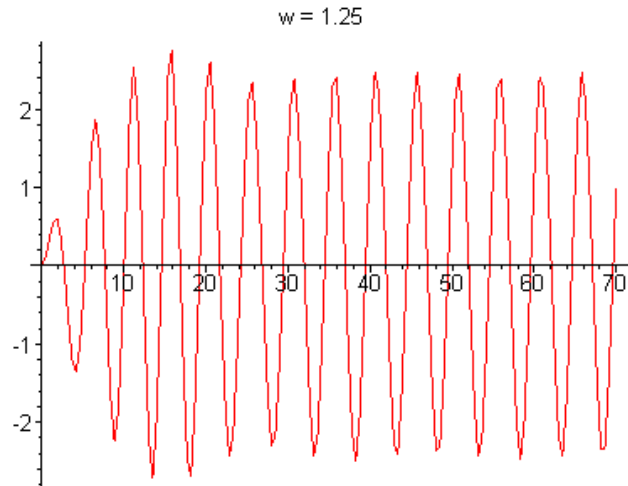


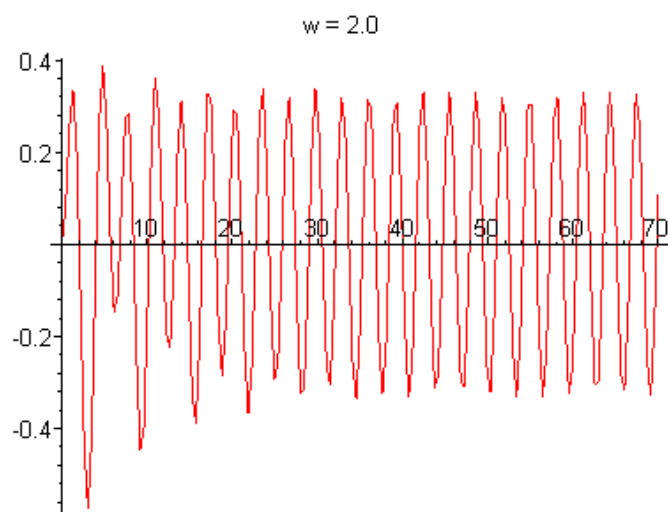
24.



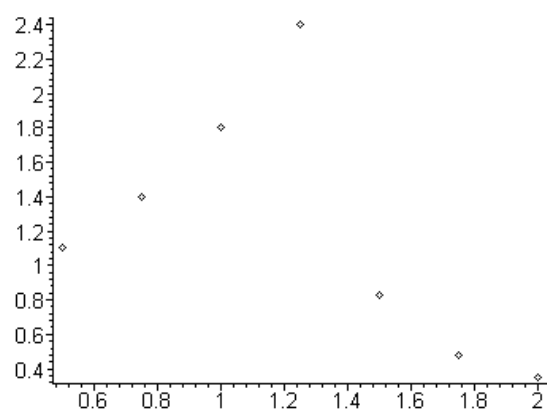
25(a).







(b).



(c). The amplitude for a similar system with a *linear* spring is given by

$$R = \frac{5}{\sqrt{25 - 49\omega^2 + 25\omega^4}}.$$

