

# Drag and 3D wings

## 1 Definitions

$D_{profile}$  = Profile drag ( $N$ )

$D_{friction}$  = Friction drag( $N$ )

$D_{pressure}$  = Pressure ( $N$ )

$c_{d,profile}$  = Profile drag coefficient for unit length (dimensionless)

$c_{d,f}$  = Friction drag coefficient for unit length (dimensionless)

$c_{d,p}$  = Pressure drag coefficient for unit length (dimensionless)

$D_{wave}$  = Wave drag( $N$ )

$D$  = Total drag ( $N$ )

$c_{d,w}$  = Wave drag coefficient for unit length (dimensionless)

$c_d$  = Drag coefficient for unit length (dimensionless)

$\alpha$  = Angle of attack (deg)

$\alpha_{eff}$  = Effective angle of attack (deg)

$\alpha_i$  = Induced angle of attack (rad)

$D_i$  = Induced drag ( $N$ )

$L$  = Lift ( $N$ )

$C_L$  = Lift coefficient (dimensionless)

$A$  = Aspect ratio (dimensionless)

$b$  = Wing span ( $m$ )

$c$  = Wing chord length ( $m$ )

$S$  = Wing area ( $m^2$ )

$q_\infty$  = Dynamic pressure in free-stream ( $Pa = N/m^2$ )

$e$  = Span effectiveness ratio (sometimes also called Oswald factor) (dimensionless)

## 2 Drag types for 2D airfoils

There are three important types of drag in aerodynamics. Skin friction drag has already been discussed in a previous chapter, and so does pressure drag due to flow separation. Together these two types of drag form the profile drag. In formula:

$$D_{profile} = D_{friction} + D_{pressure} \quad (2.1)$$

$$c_{d,profile} = c_{d,f} + c_{d,p} \quad (2.2)$$

But there is another type of drag, called wave drag. This is caused by shock waves, which are caused by supersonic velocities. So the total drag is:

$$D = D_{wave} + D_{profile} = D_{wave} + D_{friction} + D_{pressure} \quad (2.3)$$

$$c_d = c_{d,w} + c_{d,f} + c_{d,p} \quad (2.4)$$

### 3 Induced Drag

Induced drag doesn't occur in 2-dimensional airfoils. In 3-dimensional airfoils it does appear. And since airplanes have 3-dimensional airfoils, it plays an important role. It usually occurs that the local flow direction of the air differs from the relative wind. Therefore the effective angle of attack  $\alpha_{eff}$  is smaller than the geometric angle of attack  $\alpha$ . Their difference is  $\alpha_i$ , the induced angle of attack. In formula:

$$\alpha_i = \frac{\pi}{180}(\alpha - \alpha_{eff}) \quad (3.1)$$

Note that a conversion factor is necessary. This is because  $\alpha_i$  is in radians (this is necessary for equation 3.3), while the normal angle of attack is in degrees.

Geometrically it can be shown that:

$$D_i = L \sin \alpha_i = L \alpha_i \quad (3.2)$$

The latter part of the equation is an approximation, since  $\alpha_i$  is very small, and therefore  $\sin \alpha_i \approx \alpha_i$ . For elliptical lift distribution, which is often approximately the case for airplanes, the following formula is true for incompressible flows:

$$\alpha_i = \frac{C_L}{\pi A} \quad (3.3)$$

Where the aspect ratio  $A$  is equal to the 'slenderness' of the wing  $\frac{b}{c}$ . However,  $c$  is not constant along the wing, so aerodynamicists therefore have defined the aspect ratio as:

$$A = \frac{b^2}{S} \quad (3.4)$$

Combining previous equations results in:

$$D_i = L \frac{C_L}{\pi A} = q_\infty S \frac{C_L^2}{\pi A} \quad (3.5)$$

So now the induced drag coefficient can be found:

$$C_{D,i} = \frac{C_L^2}{\pi A} \quad (3.6)$$

However, elliptical lift distributions aren't always the case. Therefore, the span efficiency factor  $e$  (also sometimes called Oswald factor) has been defined, such that:

$$C_{D,i} = \frac{C_L^2}{\pi A e} \quad (3.7)$$

Now let's calculate the total drag coefficient for the wing. We don't know the induced drag for supersonic speeds, so for (low) subsonic speeds, the following equation holds:

$$C_D = c_{d,profile} + \frac{C_L^2}{\pi e A} = c_{d,f} + c_{d,p} + \frac{C_L^2}{\pi e A} \quad (3.8)$$

### 4 Slope of the ( $C_L - \alpha$ ) curve

For 2D wings, the slope of the ( $C_L - \alpha$ ) curve is  $\frac{dC_L}{d\alpha} = a_0$ . This is not the case for 3D wings. Now the relation  $\frac{dC_L}{\alpha_{eff}} = a_0$  holds. Using equations 3.1 and 3.3 (the latter with a new span effectiveness factor  $e_1$ ), and solving it for  $C_L$  gives the following relation:

$$a = \frac{a_0}{1 + \frac{57.3 a_0}{\pi e_1 A}} \quad (4.1)$$

$e_1$  is in theory a different factor than  $e$ , but in practice they are approximately equal. The factor 57.3 is in fact  $\frac{180}{\pi}$ , a conversion factor that was used to convert  $\alpha_i$  to radians in the derivation of this formula.